

# Benchmark of an efficient BGK model for rarefied gas flows in full 3D geometry

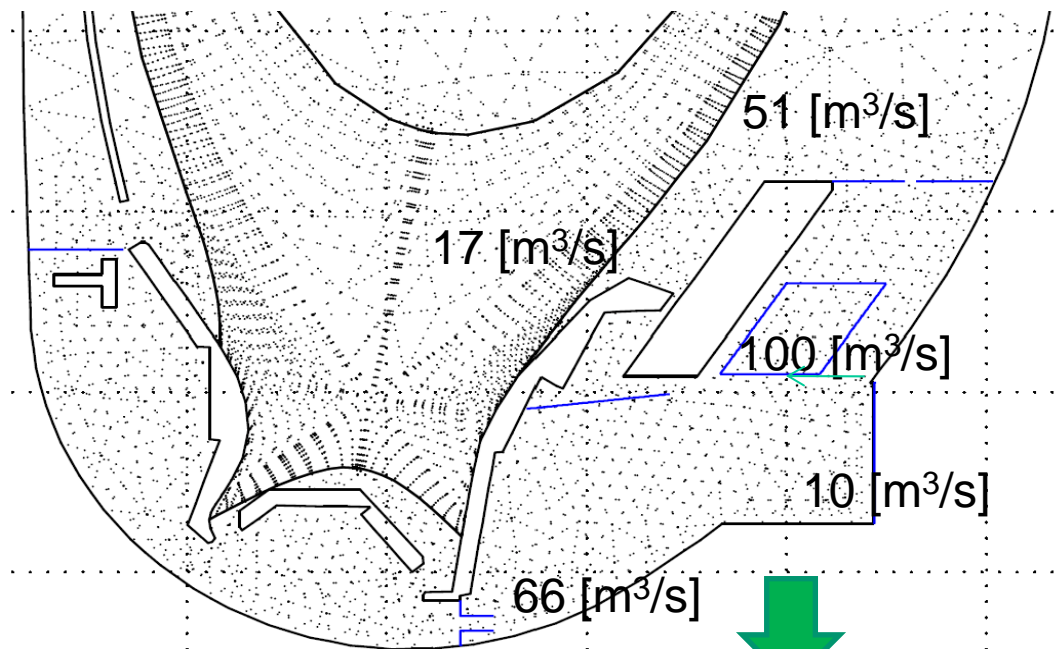
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- Introduction:
  1. basic considerations on rarefied gas flow in fusion system and related pumping
  2. conductances and flow regimes @ ASDEX Upgrade (AUG)
- Benchmark of EIRENE Monte-Carlo particles transport code (a standard in nuclear fusion) with  $\sim$  isothermal flows
  1. Numerical method using EIRENE
  2. Set up of numerical experiments
  3. Test cases:
    - a) A channel length scan in free molecular regime
    - b) Pressure scan for a slit and short channels
    - c) Pressure scan for a orifice and pipes
- Prospective and conclusions

## By-passes measurements



- The AUG poloidally and toroidally distributed ducts (3D) can be mimed in EIRENE with poloidally distributed (2D) (and toroidally uniform) ducts preserving the total effective conductance in free molecular regime

model	AUG ducts measurements	Best match EIRENE model
Main chamber to pump chamber	51 $\text{m}^3/\text{s}$	51 $\text{m}^3/\text{s}$
Divertor to pump chamber	17 $\text{m}^3/\text{s}$	17 $\text{m}^3/\text{s}$
Sub-divertor to pump chamber	66 $\text{m}^3/\text{s}$	50 $\text{m}^3/\text{s}$
Total	134 $\text{m}^3/\text{s}$	118 $\text{m}^3/\text{s}$

Range of $K_n$	Flow regime	Governig eq.	AUG regime
$K_n < 10^{-3}$	Fluid-continuum	Euler, Navier-Stokes	None
$10^{-3} < K_n < 10^{-1}$	Slip	Navier-Stokes with slip flow	#25681, $K_n = 0.027$
$10^{-1} < K_n < 10$	Transition	Boltzmann	L-mode, H-mode $K_n \geq 0.1$
$10 < K_n$	Free molecular (FMR)	Boltzmann with no collision	Low density L-mode $K_n \leq 25$

- Not only future devices but even today's exp. (AUG, C-Mod) are often in transition regime!
- But EIRENE tested only for Couette flow ...

Solves multi-species Boltzmann equation in BGK approximation for neutrals:

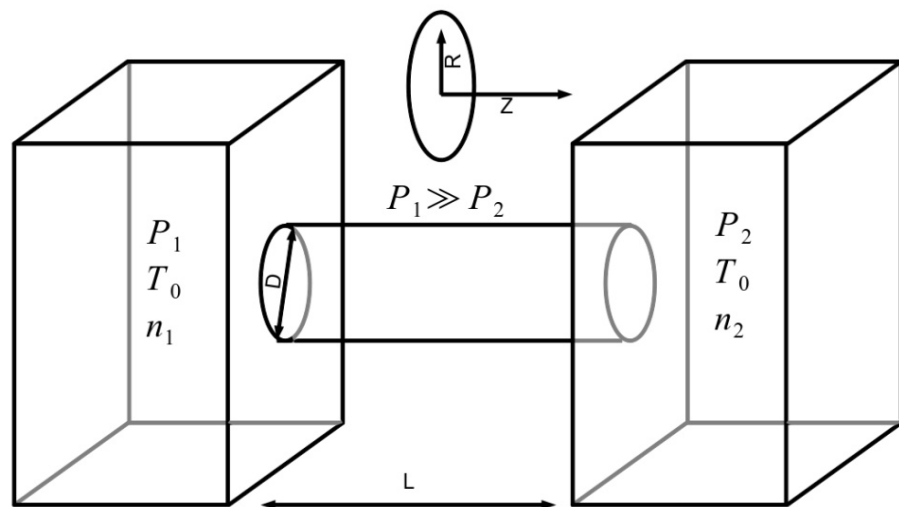
$$\frac{df_i}{dt} = \nu_i (f_M - f_i)$$

- Solution by „*successive linearisation*“ [1]:
  - Test particle trajectories are simulated and from the test particle distribution, new moments are derived for the Maxwellian of the next iteration
  - Iterations are repeated until equilibrium is reached either by fixing upstream density of influx of particles
- Sampling the trajectories of the neutral particles (H, H<sub>2</sub>, He, C...) in a given background of plasma and neutral particles. Cartesian, triangular or tetrahedral grids. Designed specially for fusion applications (definition of sources, coupling to plasma codes etc.)

[1] Reiter D., May Ch., et. al, J. Nucl. Mater, **241-243, 342 (1997)**

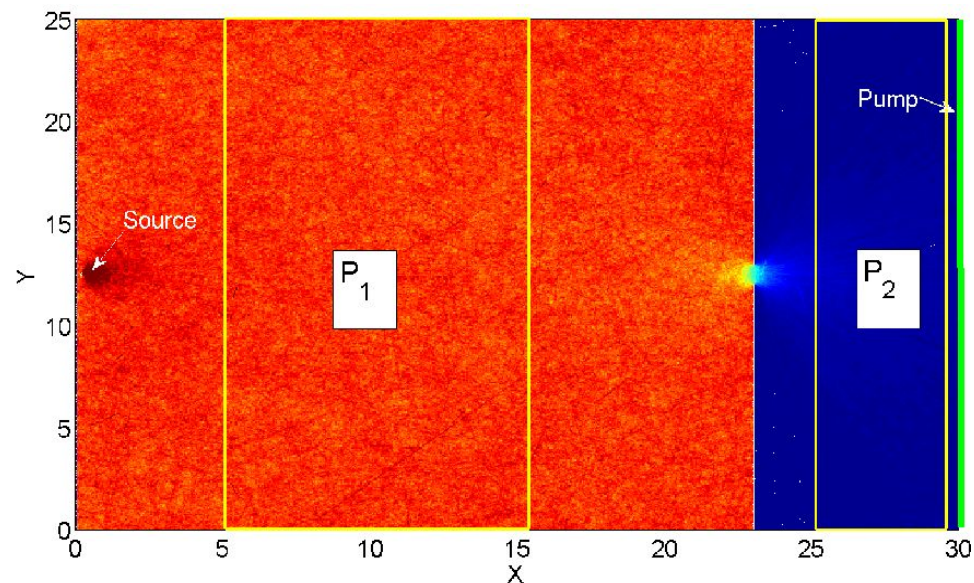
- $f_M$  is a drifting Maxwellian (equilibrium solution), depending on local moments of  $f$  in order to ensure particle, momentum and energy conservation
- $\nu_i$  are collision rates deduced from experimental viscosity
- Complex 3D geometry (divertor, bypasses etc...) can be handled.
- Can take into account collisions with wall, ionization, dissociation, charge-exchange, elastic collisions etc.
- In this benchmark purely diffusive b.c. and He gas are used .

# Problem and set up



$$C = \frac{\frac{\partial N}{\partial t}}{n_1 - n_2} \quad \text{conductance}$$

$$\delta = \frac{p_1 L}{\mu v_0} = \frac{\sqrt{\pi}}{2k_n} \quad \text{rarefaction parameter}$$



- Aperture Geometries:
  - ❖ Slit and short channels
  - ❖ Orifice and short circular tube

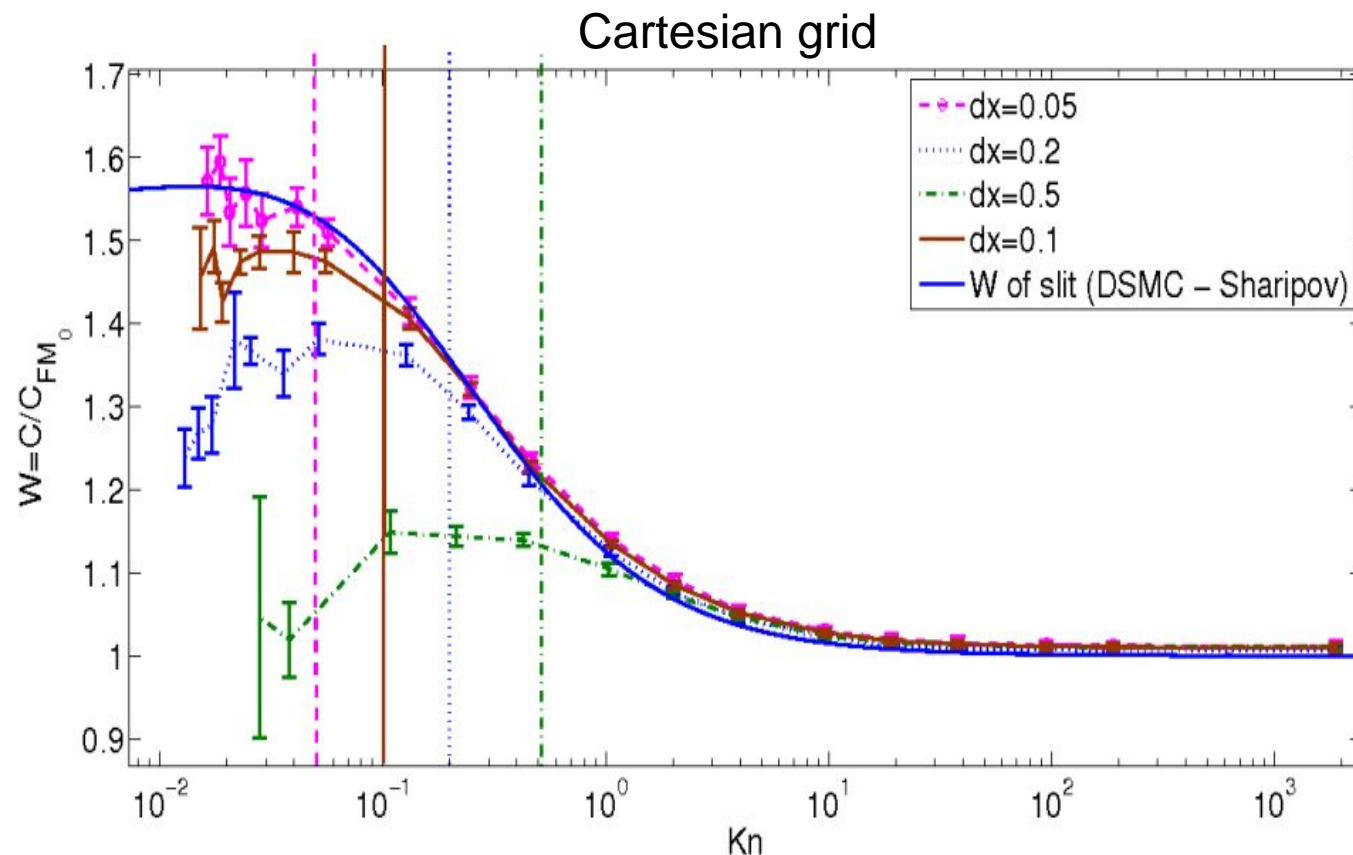
# Choosing the grid

- For

$$k_n < \frac{\Delta x}{\lambda_{mfp}}$$

meanfreepath  
< cell-size

=> gradients can not  
be resolved  
=> unphysical solution



In this work grid limits to  $k_n > 0.02$ ,  $\delta < 40-50$



# Channel length scan in FMR

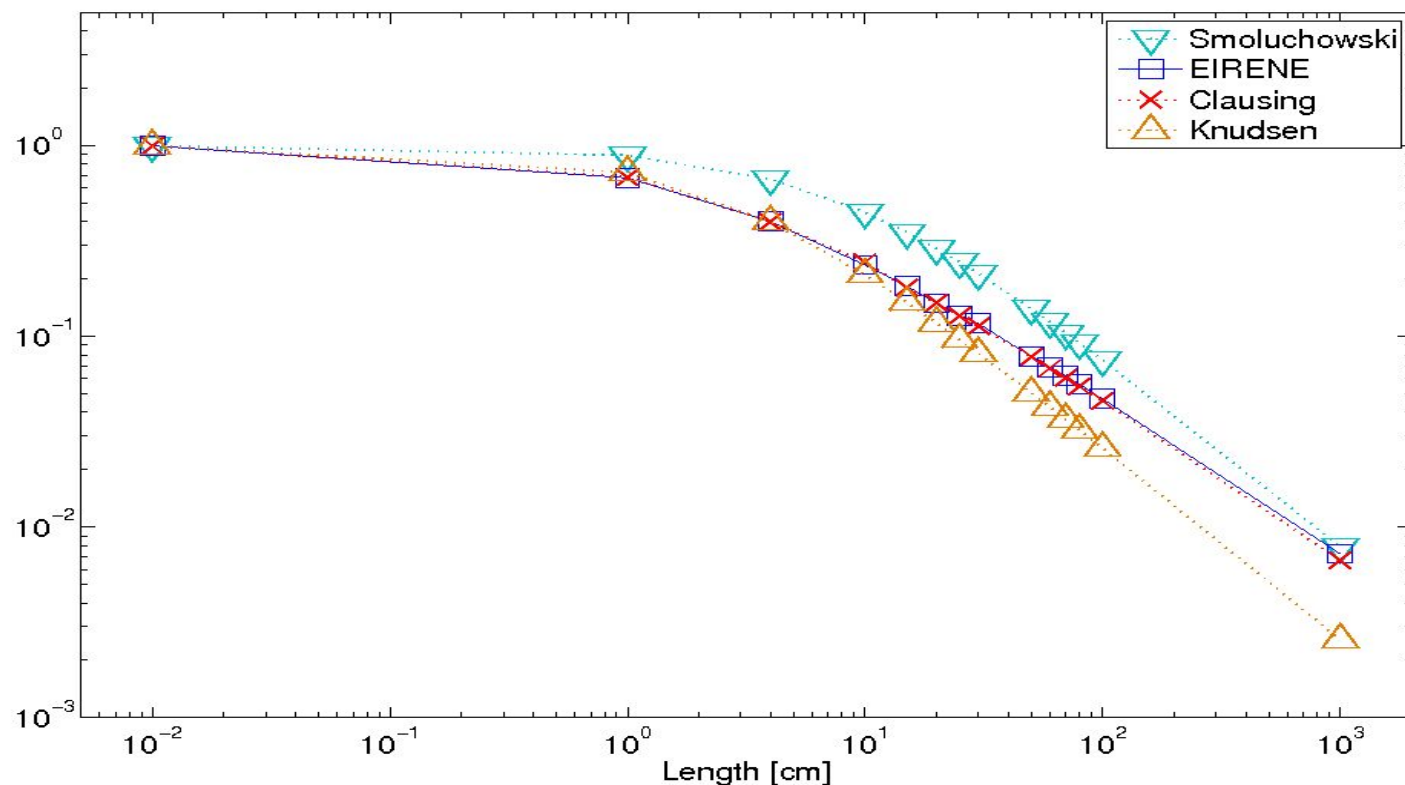
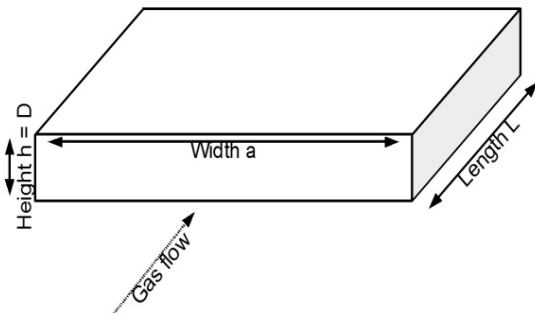
$$C_{FM} = \left( \frac{1}{1/C_{FM,0} + 1/C_{\infty-length}} \right)^{-1}$$

$$C_{FM,0} = \frac{1}{4} n v_a$$

$$C_{\infty-length} = \begin{cases} Knudsen^1 \\ Smoluchows ki^1 \end{cases} \quad W = C_{FM}/C_{FM,0}$$

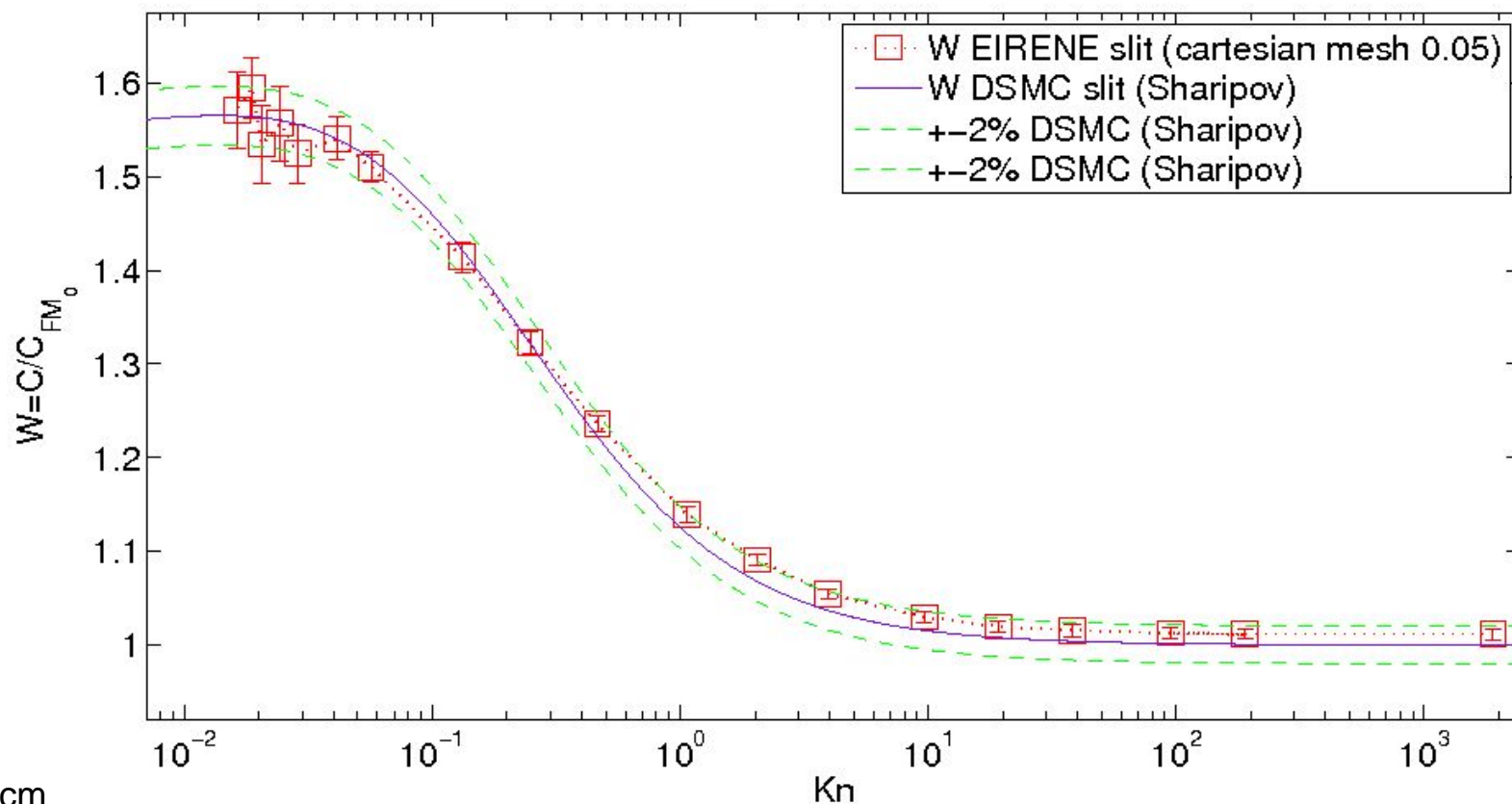
Height  $h=1\text{cm}$

Reservoir volume =  $1\text{m} \times 1\text{m} \times 10\text{m}$



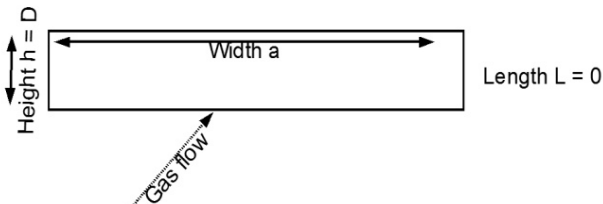
- Agreement within 0.3%, limited by statistic only

[1] J.M. Lafferty. Foundations of Vacuum Science. John Wiley and Sons, Inc., 1998



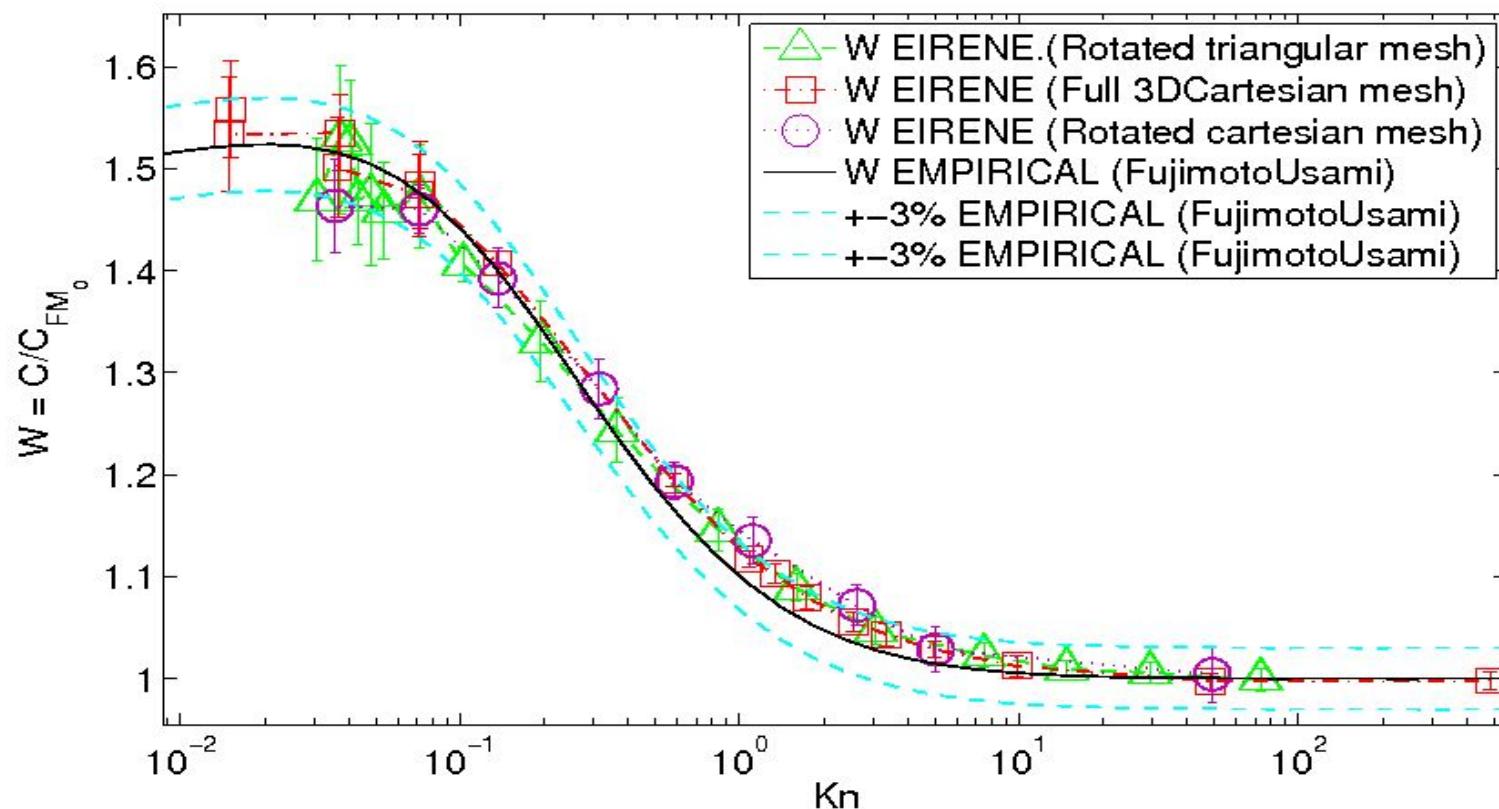
Height  $h=1\text{cm}$

Reservoir volume  $=60 \times 60 \times 60 \text{cm}^3$



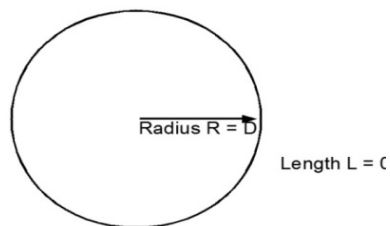
- Overall agreement with DSMC<sup>1</sup> simulations within 2%

[1] Felix Sharipov, Dalton V. Kozak. Rareed gas ow through a thin slit into vacuum simulated by the Monte Carlo method over the whole range of the Knudsen number. American Vacuum Society, 2009.



Radius  $R=0.5\text{cm}$

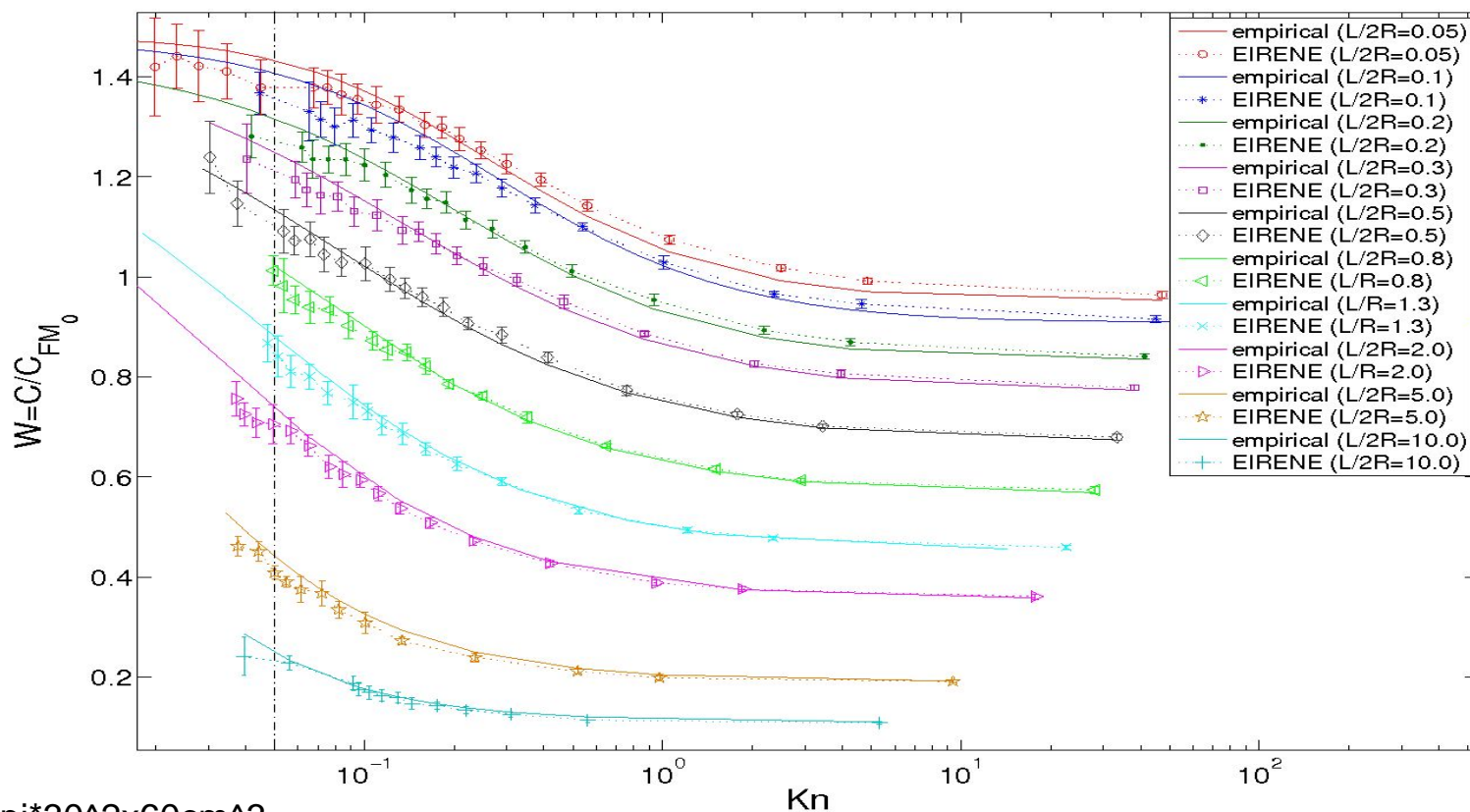
Reservoir volume  $=\pi \cdot 30^2 \times 60 \text{cm}^3$



- Agreement with experimental data within 3%

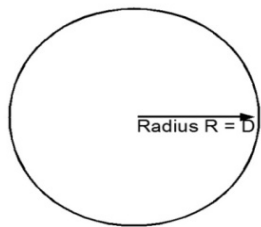
Ref: T. Fujimoto, M. Usami. Rarefied Gas Flow Through a Circular Orifice and Short Tubes. Journal of Fluids Engineering, 106, 1984.

# Short pipes



Radius  $R=0.5\text{cm}$

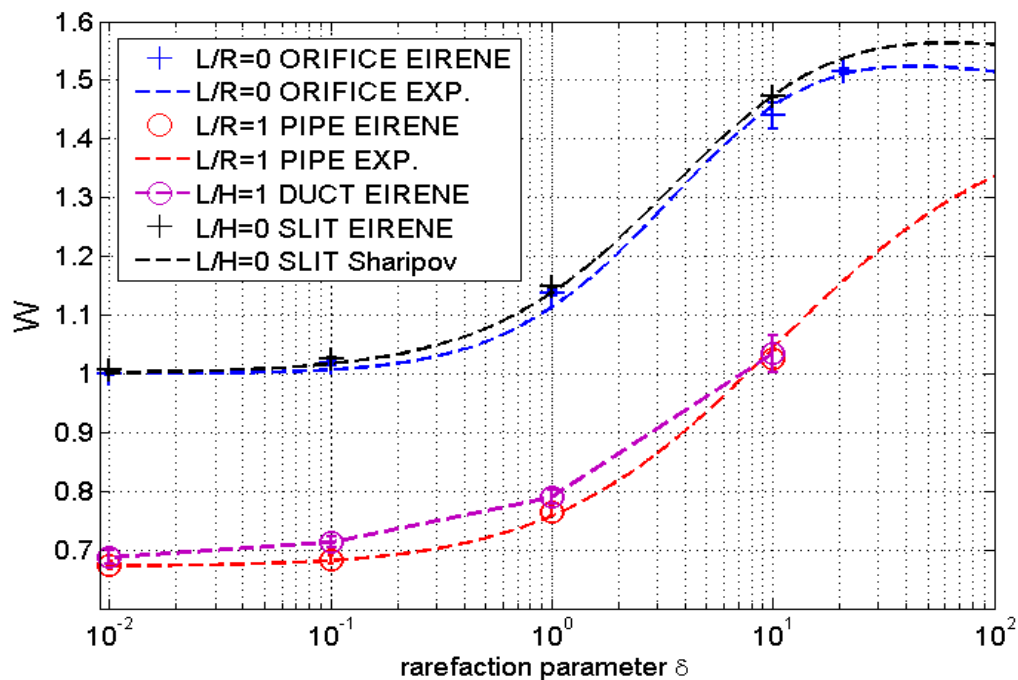
Reservoir volume  $=\pi \cdot 30^2 \cdot 60\text{cm}^3$



Length  $L = \ell$

- Agreement with experimental data within 5%

Ref: T. Fujimoto, M. Usami. Rarefied Gas Flow Through a Circular Orifice and Short Tubes. Journal of Fluids Engineering, 106, 1984.



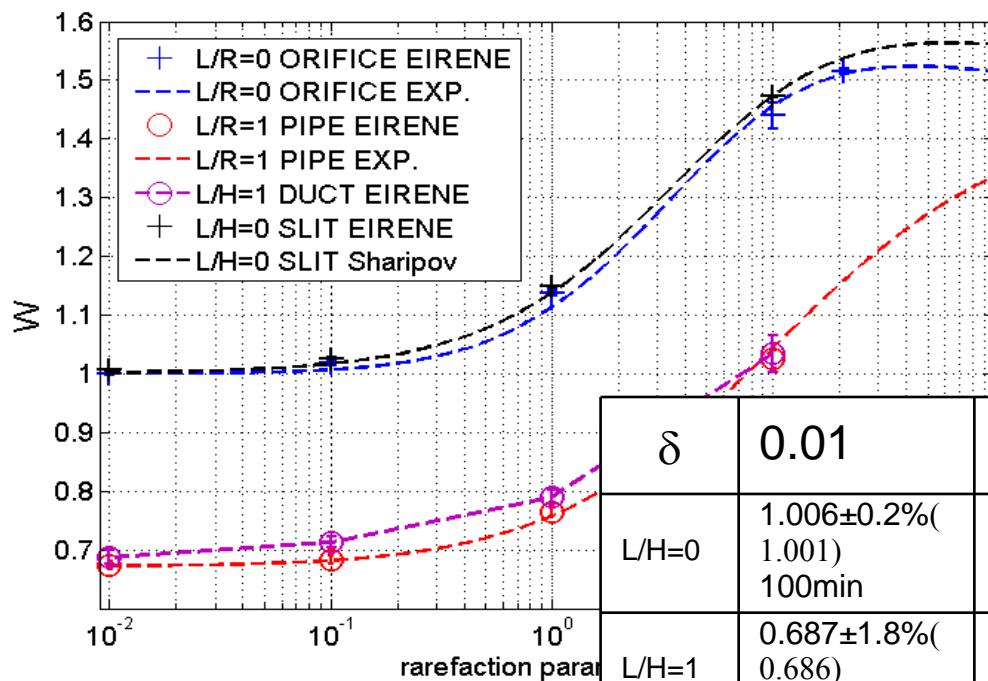
- Runs with higher statistic with parallelized version to check accuracy and performances
- **Max. difference with DSMC is 3.5% for  $\delta=10$  in L/R=1 circular pipe**

W EIRENE (Sharipov)  
1 CPU time [s]

- $\delta=100$  not clearly converged likely due to grid

Circular pipe

$\delta$	0.01	0.1	1	10	100
L/R=0	1.000±0.4% (1.001) 60min	1.018±0.3% (1.014) 200min	1.138±0.4% (1.129) 730min	1.440±1.5% (1.462) 1000min	1.509±5.5% (1.534) >10000min
L/R=1	0.673±1% (0.673) 60min	0.683±1% (0.680) 160min	0.765±1% (0.754) 466	1.025±1.5% (1.062) 3000min	



- Runs with higher statistic with parallelized version to check accuracy and performances
- **Max. difference with DSMC is 3.5% for  $\delta=10$  in L/R=1 circular pipe**

Slit and short channel

$\delta$	0.01	0.1	1	10	100
L/H=0	1.006±0.2% (1.001) 100min	1.026±0.2% (1.026) 200min	1.148±0.4% (1.148) 400min	1.472±1% (1.479) 4000min	
L/H=1	0.687±1.8% (0.686) 100min	0.713±1.3% (0.698) 300min	0.789±1.5% (0.767) 480min	1.034±3% (1.038) 2000min	

Circular pipe

$\delta$	0.01	0.1	1	10	100
L/R=0	1.000±0.4% (1.001) 60min	1.018±0.3% (1.014) 200min	1.138±0.4% (1.129) 730min	1.440±1.5% (1.462) 1000min	1.509±5.5% (1.534) >10000min
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W EIRENE (Sharipov)  
1 CPU time [s]

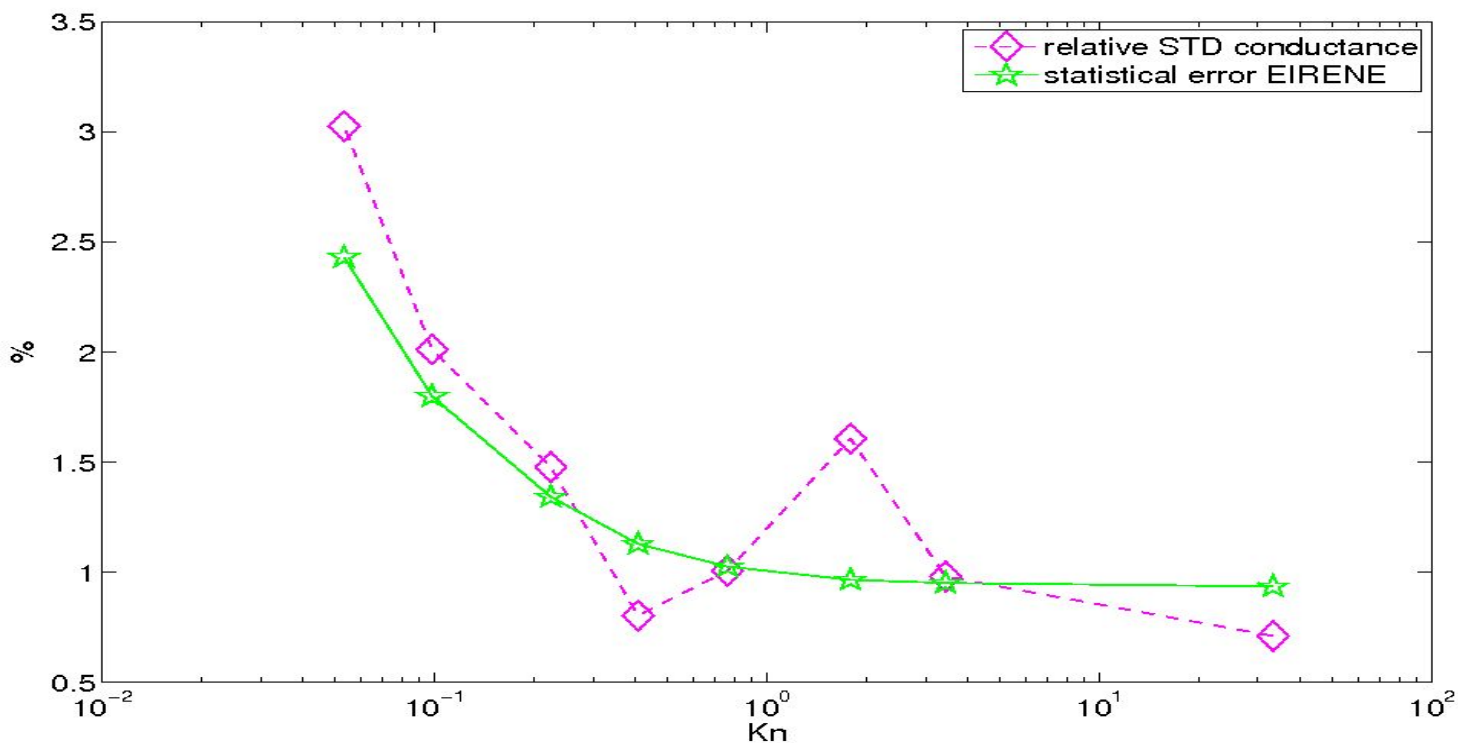
- $\delta=100$  not clearly converged likely due to grid

- Non-linear BGK agrees for  $\delta < 30$  within 5% relative to DSMC and experiments
- Choice of the grid is crucial, no clear recipe yet
- Code not optimised for this task, but still it is very efficient for transition regime (about 8h for  $\delta \sim 1$ ). And complex 3D geometry can be handled!
- Current development:
  - Use ES-BGK for correct  $P_r$  number
  - Optimise grids for  $\delta$  up to 100
  - Understand better convergence properties

# Back up slides

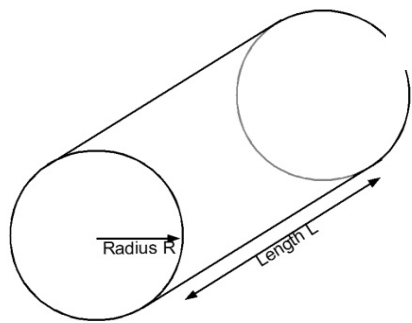
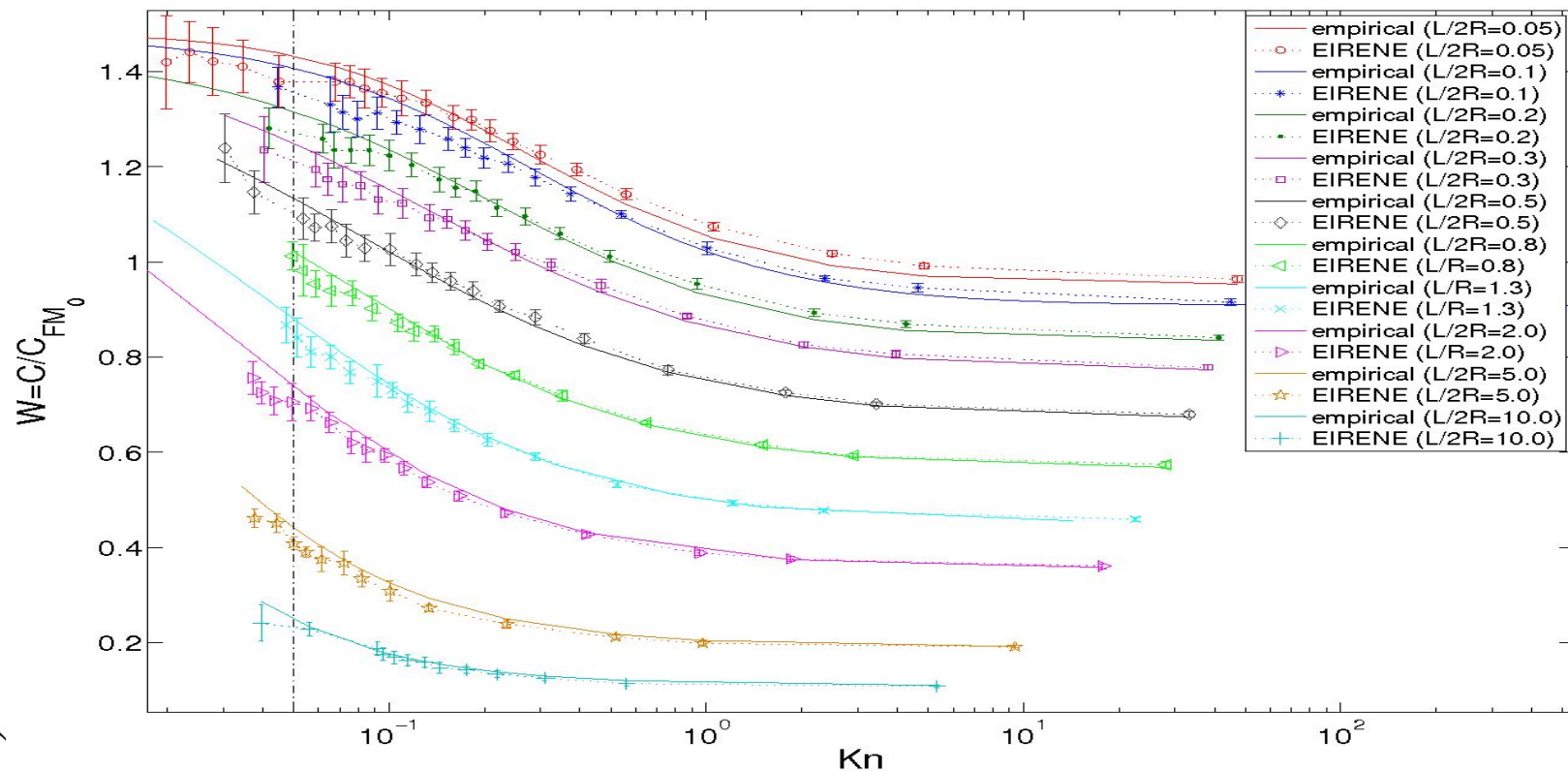


# Statistical error



- STD of converged runs used as error estimator
- STD match statistical error resulting from Monte Carlo procedure

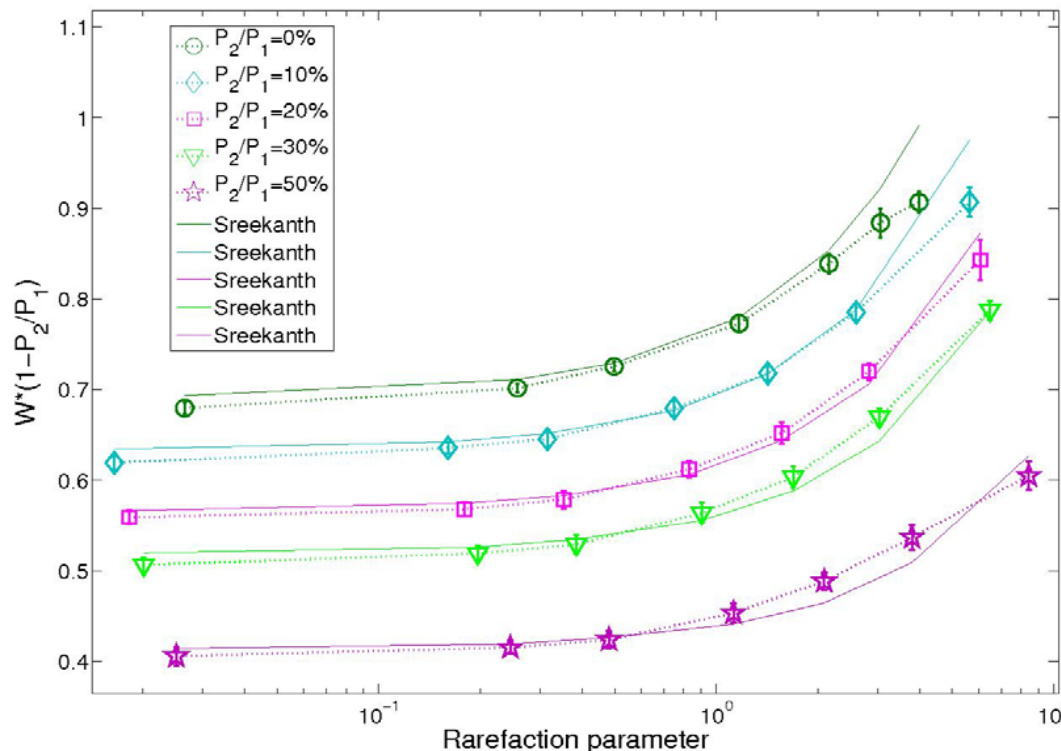
# Pipes length scan



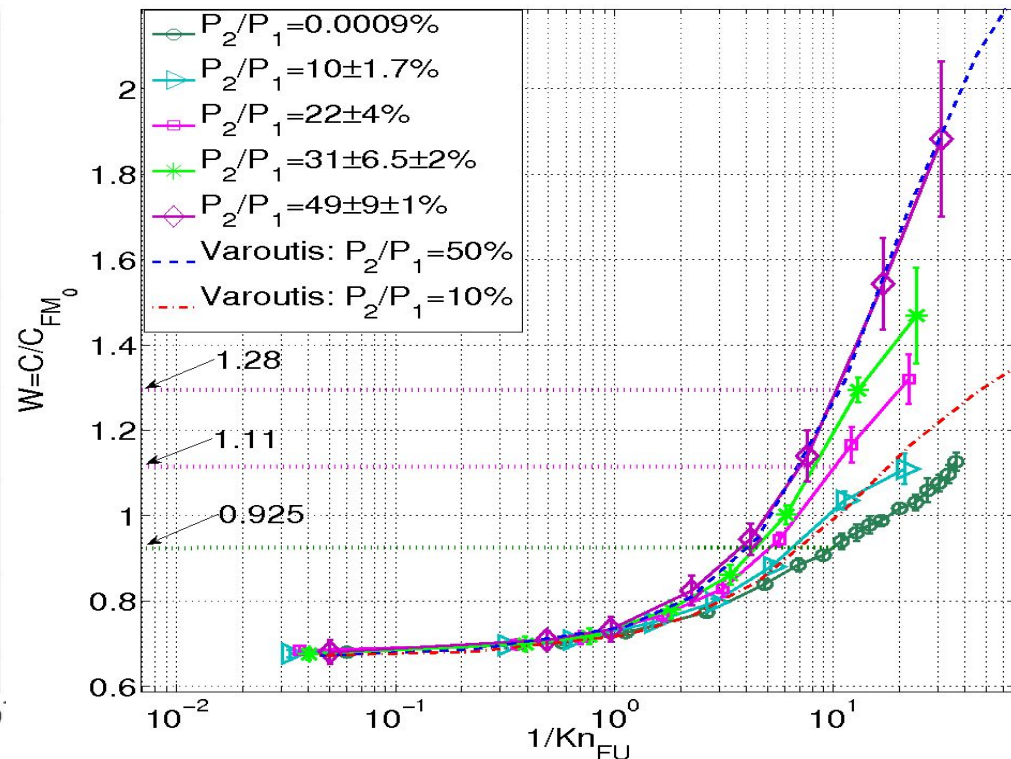
- Agreement within 5%

Ref: Tetsuo Fujimoto, Masaru Usami. Rareed Gas Flow Through a Circular Orifice and Short Tubes. Journal of Fluids Engineering, 106, 1984.

# Pressure ratio scan

Circular tube with  $L/R=1$ 

Ref: A.K.Sreekanth. Transition ow through short circular tubes.  
The Physics of  
Fluids, 1965.

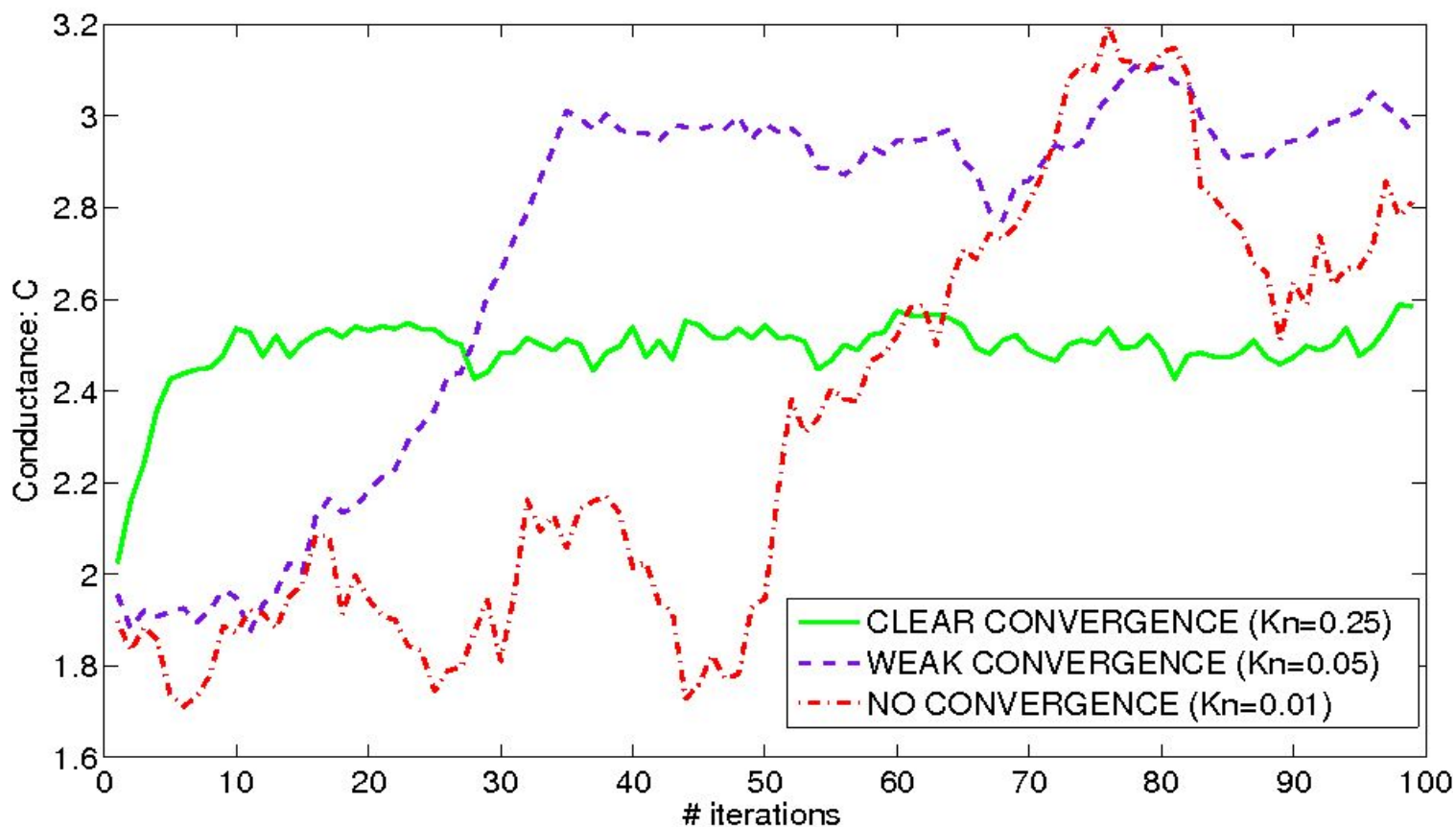
Circular tube with  $L/R=1$ 

Ref: S.Varoutis, D.Valougeorgis, F.Sharipov. Simulation of gas  
flow through tubes of finite length over the whole range of  
rarefaction for various pressure drops ratios. Journal of Vacuum  
Science and Technology, 2009.

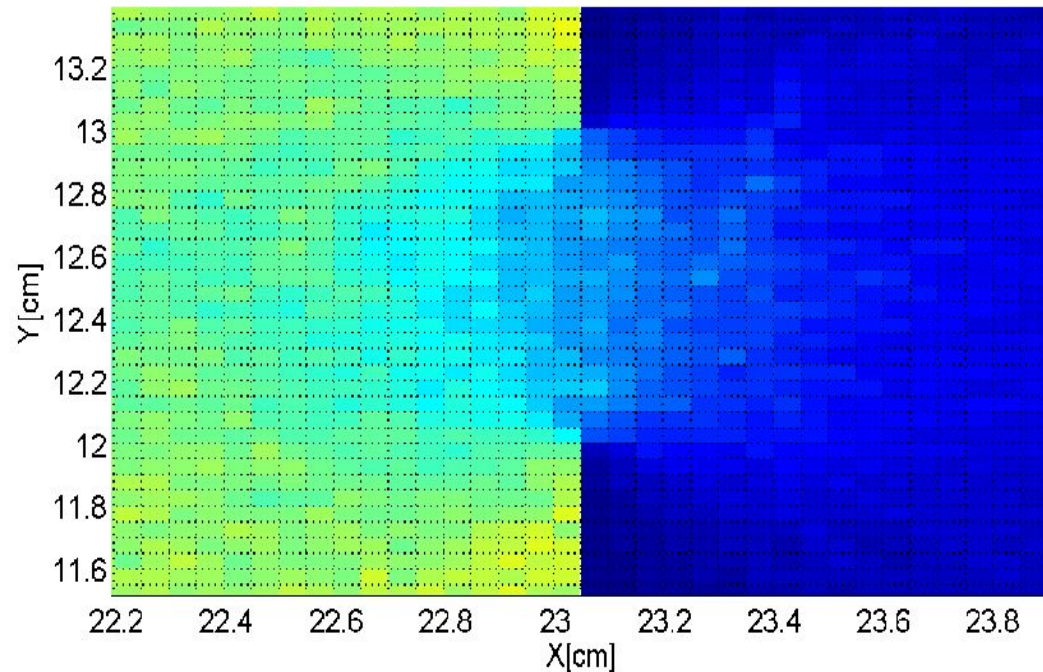
Agreement within 5% for  $Kn > 0.1$

# Convergence

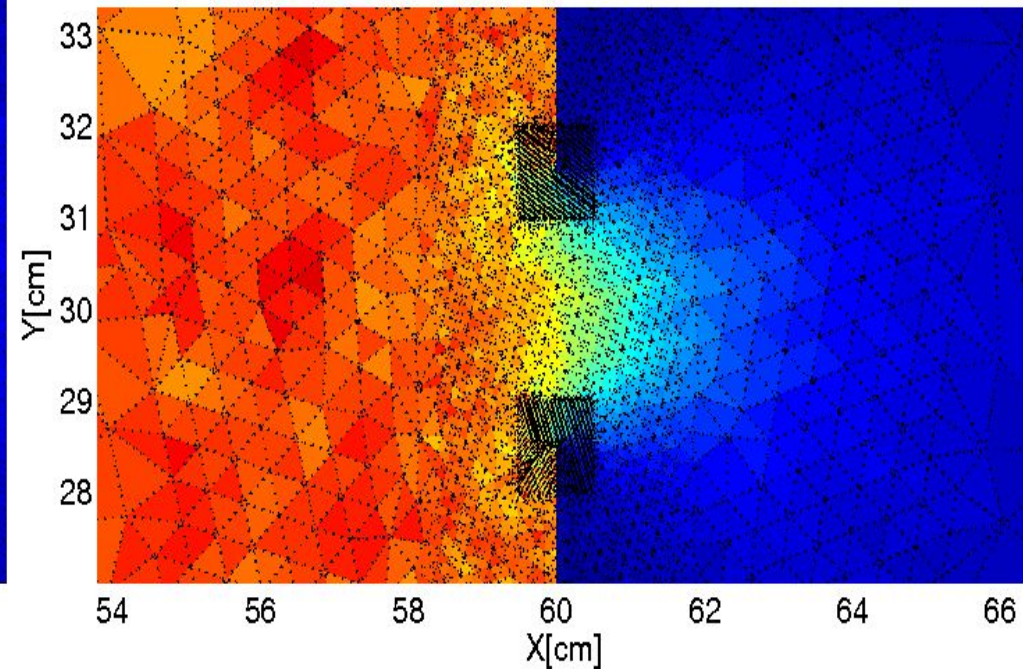
Convergence depends on grid resolution, statistics and Kn







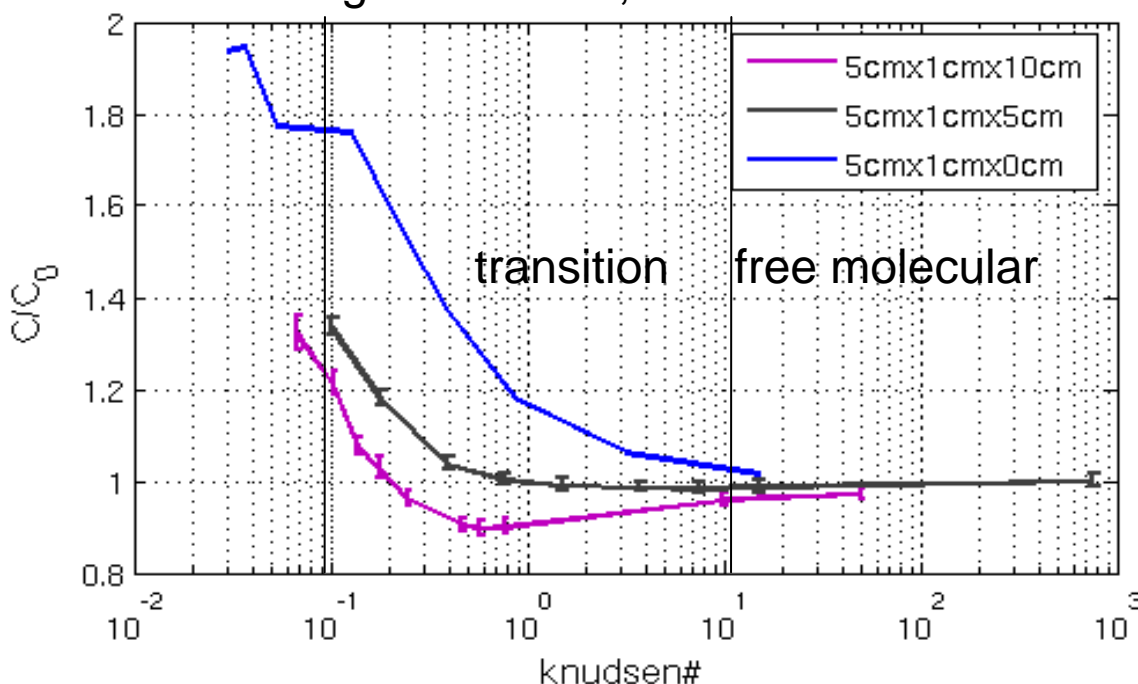
Cartesian mesh



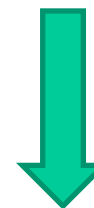
Triangular mesh

3D grids are generated by rotation or extension perpendicular to the plane

Duct length scan  $L=0, 5$  and  $10$  cm



- Qualitative trends are:
  1. Long(short) duct/pipe (do not )show the Knudsen minimum
  2. Strongly rectangular/elliptical duct show deeper minimum
  3. Round/squared pipe/duct show “flat” behaviour near  $K_n=1$ .



- The conductance of AUG rectangular short ducts should be about 10% larger at  $K_n=1$  and 40-80% larger at  $K_n=0.1$
- Detailed calculation for AUG ducts geometry will be performed in the near future

$$\frac{df_i}{dt} = \sum_{j=i} \nu_{ij} \cdot \left( f_M^{ij} - f_i \right)$$

$f_M^{ij}$ : shifted Maxwellian  
 $\nu_{ij}$ : velocity independent

$$n_{ij} = n_j, \quad \mathbf{u}_{ij} = \frac{m_i \mathbf{u}_i + m_j \mathbf{u}_j}{m_i + m_j}, \quad T_{ij} = T_i - \frac{2 \cdot m_i m_j}{(m_i + m_j)^2} \left[ (T_i - T_j) - \frac{m_j}{6k} (\mathbf{u}_i - \mathbf{u}_j)^2 \right]$$

